

Replacement of Bridge 30 (SR-87 Over Lagoon Creek Overflow)

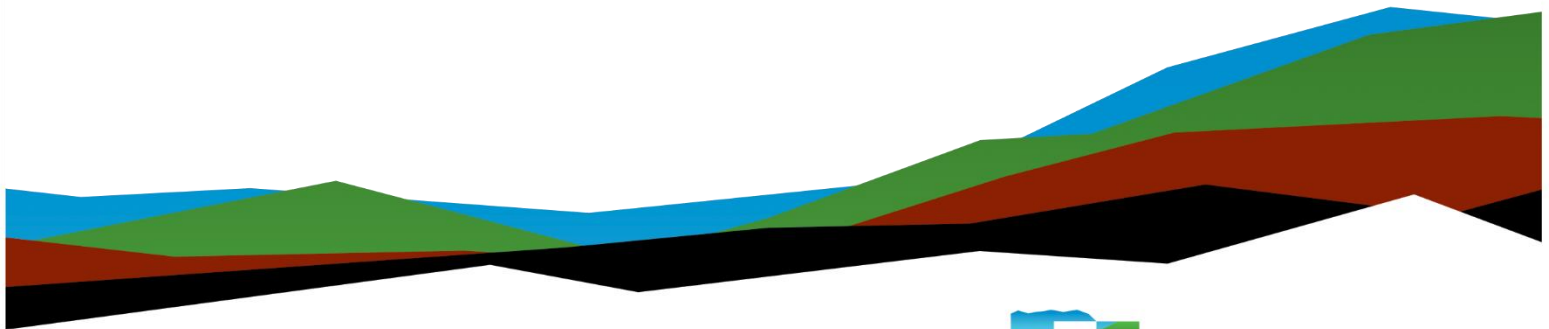
Geotechnical Data Report

Haywood County, Tennessee

August 15, 2025 | Terracon Project No. 1A255072

Prepared for:

American Structurepoint Inc.
600 Superior Ave East, Suite 2401
Cleveland, Ohio 44114



Nationwide
Terracon.com

- Facilities
- Environmental
- Geotechnical
- Materials



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August 15, 2025

American Structurepoint Inc.
600 Superior Ave East, Suite 2401
Cleveland, Ohio 44114

Attn: Mr. Gabe Liptak, P.E.
P: (216) 302-3694
E: gliptak@structurepoint.com

Re: Geotechnical Data Report
Replacement of Bridge 30 (SR-87 Over Lagoon Creek Overflow)
Haywood County, Tennessee
Terracon Project No. 1A255072

Dear Mr. Liptak:

We have completed the scope of work for the above referenced project. This Data Report presents the findings of the subsurface exploration, including field and laboratory test results.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report or if we may be of further service, please contact us.

Sincerely,

Terracon

Eric Conway, P.E.
Geotechnical Department Manager

James Vinson, P.E.
National Manager

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Introduction

This report presents the results of our subsurface exploration performed for the proposed bridge replacement along SR-87 in Haywood County, Tennessee. The geotechnical Scope of Services included the advancement of test borings, laboratory testing, geophysical testing and preparation of this data report. The exploratory locations were determined by Terracon field staff. Encountered soil and groundwater depths are provided herein.

Site Information

The following description of site conditions is derived from our site visit in association with field exploration and our review of publicly available geologic and topographic maps.

Item	Description
Site Information	The approximate coordinates for the bridge crossing are as follows: ■ Bridge No. 30: 35.6318° N 89.4131° W See Site Location
Current Ground Cover	Away from the existing bridge, SR-87 pavement consists of asphalt overlaying fill.
Existing Topography (Estimated using Google Earth)	The ground surface elevation at the borings is approximately 295 feet.

Geologic Formations

Formation ¹	Description
Alluvial Deposits	Sand, silt, clay, and gravel. Flood plain of Mississippi River, more than 100 feet thick.
¹ . Geologic Map of Tennessee, published by the State of Tennessee Department of Conservation, Division of Geology (1966).	

Geotechnical Borings and Laboratory Testing

Terracon drilled two borings near the proposed bridge replacement. Each boring encountered asphalt over fill over alluvial deposits.

Subsurface conditions observed at each location are indicated on the individual logs. The individual logs can be found in the [Exploration Results](#). Drawings depicting site locations and boring locations relative to existing site features are attached.

Laboratory testing was performed to confirm visual descriptions and further characterize the encountered soils. Testing included the following: natural moisture, grain-size distribution, Atterberg limits, compaction, California Bearing Ratio, unconsolidated-undrained triaxial and corrosion series. Test results are attached with the boring logs.

Seismic Survey

Terracon performed a limited seismic survey consisting of twenty-two Multi-Channel Analysis of Surface Waves (MASW) arrays at the subject bridge site to obtain shear wave velocities of the soil within the upper 100 feet. Results of the seismic survey as well as location map for the arrays are attached.

General Comments

This geotechnical data report does not include any analysis or recommendations. The data presented in this report are based upon the borings and geophysical data at the indicated locations. This report does not reflect variations that may occur across the site, or due to the modifying effects of weather. The nature and extent of such variations may not become evident until, during, or after construction.

No warranties, either expressed or implied, are intended or made. The scope of geotechnical services does not include either specifically or by implication any environmental assessment of the site or identification or prevention of pollutants, hazardous materials, or conditions.

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Attachments

Exploration and Testing Procedures

Field Exploration

Number of Exploration Points	Approximate Exploration Depth (feet)	Location
2	100	Bridge Abutments
2 MASW Arrays	100	Bridge Abutments

Boring Layout and Elevations: Terracon personnel provided the boring layout using handheld GPS equipment (estimated horizontal accuracy of about ±10 feet) and referencing existing site features. Approximate ground surface elevations were estimated using Google Earth™.

Subsurface Exploration Procedures: We advanced the borings with an truck-mounted rotary drill rig using continuous flight solid stem augers and rotary wash boring techniques as necessary depending on soil conditions. Three samples were obtained in the upper 10 feet of each boring and at intervals of 5 feet thereafter. In the thin-walled tube sampling procedure, a thin-walled, seamless steel tube with a sharp cutting edge was pushed hydraulically into the soil to obtain a relatively undisturbed sample. In the split-barrel sampling procedure, a standard 2-inch outer diameter split-barrel sampling spoon was driven into the ground by a 140-pound automatic hammer falling a distance of 30 inches. The number of blows required to advance the sampling spoon the last 12 inches of a normal 18-inch penetration is recorded as the Standard Penetration Test (SPT) resistance value. The SPT resistance values, also referred to as N-values, are indicated on the boring logs at the test depths.

We also observed the boreholes while drilling with augers for the presence of groundwater. The measured groundwater levels are shown on the attached boring logs.

The sampling depths, penetration distances, and other sampling information was recorded on the field boring logs. The samples were placed in appropriate containers and taken to our soil laboratory for testing and classification by a Geotechnical Engineer. Our exploration team prepared field boring logs as part of the drilling operations. These field logs included visual classifications of the materials observed during drilling and our interpretation of the subsurface conditions between samples. Final boring logs were prepared from the field logs. The final boring logs represent the Geotechnical Engineer's interpretation of the field logs and include modifications based on observations and tests of the samples in our laboratory.

Multi-Channel Analysis of Surface Waves: Our method of investigation utilized a standard fixed-array set of MASW geophones. Each array consisted of 24 4.5Hz

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geophones, spaced 10 feet apart along a sensor cable. For the passive surveys, ambient noise (such as nearby traffic or construction) on the site was recorded by a seismograph. For the active surveys, three sledgehammer strikes were performed every 10 feet against a polyethylene plate from 20 feet before the start of the array through geophone 12.

The data was returned to our office and processed using dispersion analysis software (SurfSeis, engineered by the Kansas Geological Survey) that extracts the fundamental-mode dispersion curve(s). The active and passive surveys performed at each line were combined to produce a broader-band overtone image to better identify the dispersion trends. The resulting curves were inverted and modeled to yield a 1D shear-wave velocity profile along the array to 100 feet below ground surface. The velocity models from the MASW surveys are presented on **Exhibit 2**.

Laboratory Testing

The project engineer reviewed the field data and assigned laboratory tests. The laboratory testing program included the following types of tests:

- Moisture Content
- Unconfined Compression
- Atterberg Limits
- Triaxial Compression
- Grain Size Analysis
- Corrosion Suite
- Standard Proctor
- California Bearing Ratio

Based on the results of our field and laboratory programs, we described and classified the soil samples in accordance with the Unified Soil Classification System.

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Site Location and Exploration Plans

Contents:

Site Location Plan
Exploration Plan

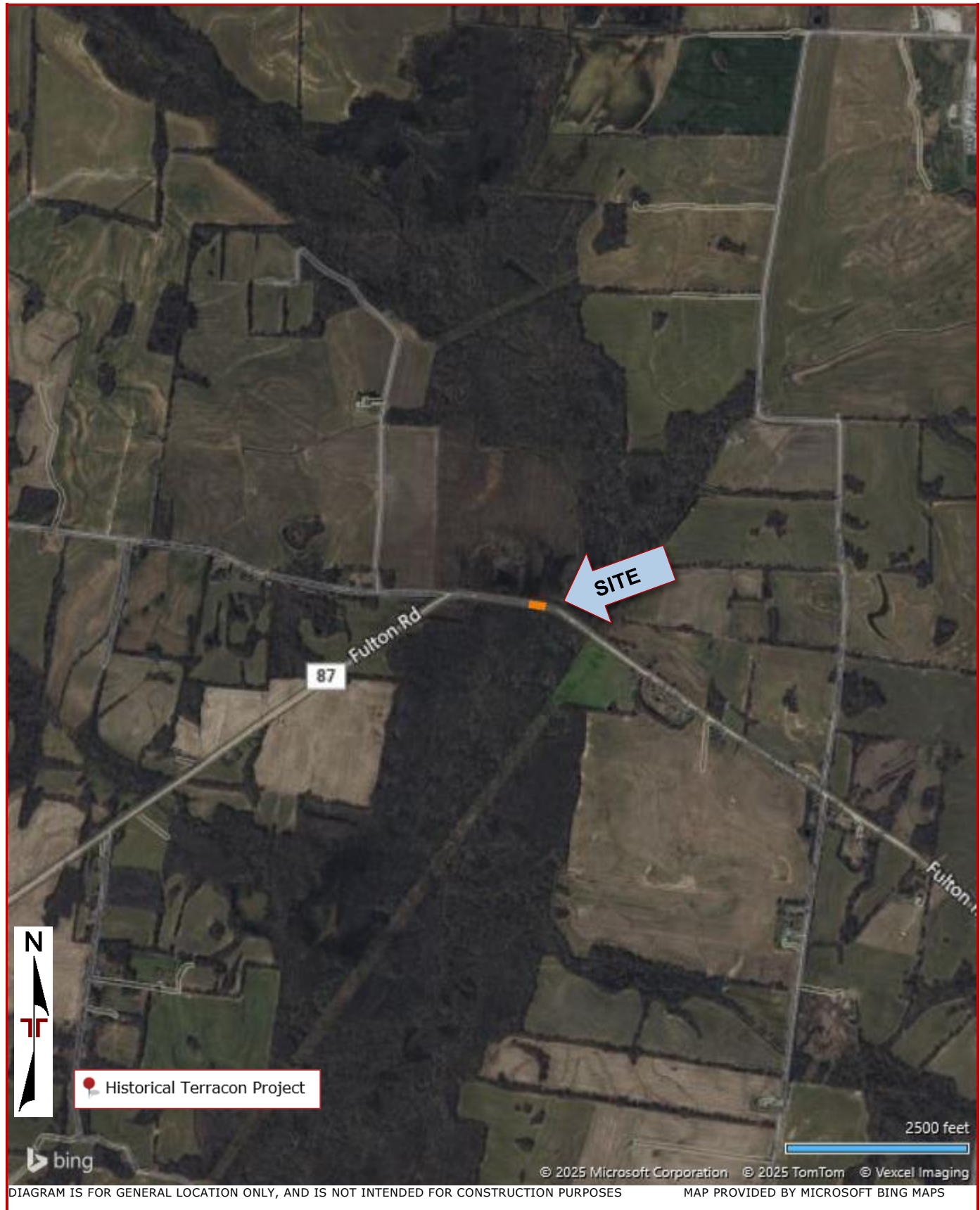
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Site Location



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Exploration Plan



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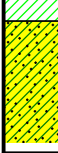


Exploration and Laboratory Results

Contents:

- Boring Logs (B-30-1 and B-30-2)
- Lab Summary
- Atterberg Limits
- California Bearing Ratio
- Standard Proctor
- Grain Size Analysis
- Triaxial Compression
- Corrosion Suite
- Geophysical Exploration Results

Boring Log No. B-30-1

Graphic Log	Location: See Exploration Plan		Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Strength Test			Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits		
	Latitude: 35.6319° Longitude: -89.4132°	Depth (Ft.)					Approximate Elevation: 295 (Ft.)	Test Type	Compressive Strength (psf)			Strain (%)	LL-PL-PI	Percent Fines
	0.3	ASPHALT	294.75											
	FILL - SILTY CLAY (CL-ML) , trace gravel, brownish gray, moist											29-22-7	98.1	
	4.5		290.5			5-5-7 N=12								
	LEAN CLAY (CL) , light gray to gray, moist, very soft to stiff					2-1-2 N=3			23.0		33-20-13			
						WOH-WOH-1 N=1			30.6					
	10						UC	23562	15	23.2	105	47-17-30	97.2	
						4-6-7 N=13								
	15				3-4-4 N=8						34-13-21			
						3-3-4 N=7			29.0					
	20	trace sand			2-3-3 N=6				26.3		28-20-8			
						3-3-4 N=7			23.5					
	25													
	hard below 28 feet					17-19-19 N=38			19.5					
	31.8		263.2											
	SANDY LEAN CLAY (CL) , gray, wet, very soft					WOH-WOH-1 N=1						59.5		
			35											

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).
See [Supporting Information](#) for explanation of symbols and abbreviations.
Elevation Reference: Elevations were interpolated from Google Earth

Notes

Water Level Observations

▽ While drilling

Drill Rig

CME 75

Hammer Type

Automatic

Driller

Terracon

Logged by

P Van Winkle

Boring Started

05-31-2025

Boring Completed

05-31-2025

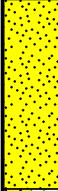
Advancement Method

Continuous Flight Auger/Mud Rotary

Abandonment Method

Boring backfilled with auger cuttings upon completion.

Boring Log No. B-30-1

Graphic Log	Location: See Exploration Plan		Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Strength Test			Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits	
	Latitude: 35.6319° Longitude: -89.4132°						Test Type	Compressive Strength (psf)	Strain (%)			LL-PL-PI	Percent Fines
	Depth (Ft.) Approximate Elevation: 295 (Ft.)												
	SANDY LEAN CLAY (CL) , gray, wet, very soft <i>(continued)</i>		36.8										
	POORLY GRADED SAND WITH CLAY (SP-SC) , fine grained sand, light gray, wet, medium dense		41.8			10-8-6 N=14			22.7			NP	10.9
	POORLY GRADED SAND (SP) , fine grained sand, light gray, wet, medium dense		46.8			7-7-7 N=14			23.1				4.9
	POORLY GRADED SAND WITH CLAY (SP-SC) , trace rounded gravel, fine grained sand, light gray, wet, loose to dense		50.0			6-15-12 N=27			18.0				5.8
			55.0			4-4-5 N=9			25.6				7.7
			60.0			5-10-11 N=21			23.8				9.7
			65.0			10-12-13 N=25			21.8				10.2
			70.0			13-17-15 N=32			23.0				9.4

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

See [Supporting Information](#) for explanation of symbols and abbreviations.

Elevation Reference: Elevations were interpolated from Google Earth

Water Level Observations

 While drilling

Drill Rig

CME 75

Hammer Type

Automatic

Driller

Terracon

Notes

Advancement Method

Continuous Flight Auger/Mud Rotary

Abandonment Method

Boring backfilled with auger cuttings upon completion.

Logged by

P Van Winkle

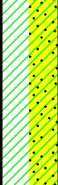
Boring Started

05-31-2025

Boring Completed

05-31-2025

Boring Log No. B-30-1

Graphic Log	Location: See Exploration Plan Latitude: 35.6319° Longitude: -89.4132°	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Strength Test			Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits	
						Test Type	Compressive Strength (psf)	Strain (%)			LL-PL-PI	Percent Fines
	Depth (Ft.) Approximate Elevation: 295 (Ft.)											
	POORLY GRADED SAND WITH CLAY (SP-SC) , trace rounded gravel, fine grained sand, light gray, wet, loose to dense (<i>continued</i>)											
	76.8 218.2	75		X	13-19-21 N=40				21.0			9.9
	CLAYEY SAND (SC) , fine grained sand, bluish gray, wet, dense											
	81.8 213.2	80		X	12-17-23 N=40				25.5			18.5
	POORLY GRADED SAND WITH CLAY (SP-SC) , trace organics, fine grained sand, bluish gray, wet, dense											
	86.8 208.2	85		X	12-16-18 N=34				22.9			9.6
	SANDY LEAN CLAY (CL) , fine grained sand, dark grayish brown, wet, hard											
	91.8 203.2	90		X	15-18-17 N=35				23.8			57.9
	LEAN CLAY WITH SAND (CL) , dark grayish brown, wet, stiff											
	96.8 198.2	95		X	3-4-5 N=9							
	SANDY LEAN CLAY (CL) , dark grayish brown, wet, stiff											
	100.0 195	100		X	3-4-10 N=14				27.2		21-14-7	67.0
	Boring Terminated at 100 Feet											

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

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Water Level Observations

 While drilling

Drill Rig

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Notes

Advancement Method

Continuous Flight Auger/Mud Rotary

Abandonment Method

Boring backfilled with auger cuttings upon completion.

Logged by

P Van Winkle

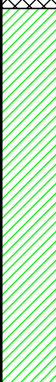
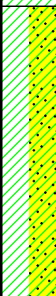
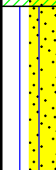
Boring Started

05-31-2025

Boring Completed

05-31-2025

Boring Log No. B-30-2

Graphic Log	Location: See Exploration Plan		Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Strength Test				Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits		Percent Fines
	Depth (Ft.)	Approximate Elevation: 295 (Ft.)					Test Type	Compressive Strength (psf)	Strain (%)	Confining Pressure (psi)			LL-PL-PI		
	0.3	ASPHALT	294.75												
	FILL - SILT (ML) , trace sand, grayish brown with brownish yellow, moist														
	4.5		290.5		X	2-2-4 N=6					27.4				
		LEAN CLAY (CL) , bluish gray to grayish brown, moist, very soft to medium stiff		5	X	WOH-2-2 N=4					26.9				
					X	WOH-WOH-WOH					29.2		32-18-14		
				10	▽										
					X	1-3-4 N=7									
	very stiff below 12 feet														
	14.5		280.5		■		UU	3923	14.8	10	24.7	103	37-18-19	93.3	
		LEAN CLAY WITH SAND (CL) , grayish brown, moist, medium stiff to stiff		15	X	3-3-4 N=7					28.3				
					X										
					X	2-4-5 N=9					26.7		31-18-13		
				20	X	3-3-3 N=6					25.7				
	22.3		272.7												
		SILT WITH SAND (ML) , grayish brown, moist, medium stiff		25	X	2-2-4 N=6					18.7		NP		
	26.8		268.2												
		POORLY GRADED SAND (SP) , fine to medium grained sand, gray, wet, medium dense		30	X	14-14-12 N=26					19.7				4.8
				35	X	5-5-6 N=11					21.5				1.2

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

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Elevation Reference: Elevations were interpolated from Google Earth

Water Level Observations

 While drilling

Drill Rig

CME 75

Hammer Type

Automatic

Driller

Terracon

Notes

Advancement Method

Continuous Flight Auger/Mud Rotary

Abandonment Method

Boring backfilled with auger cuttings upon completion.

Logged by

P Van Winkle

Boring Started

06-02-2025

Boring Completed

06-02-2025

Boring Log No. B-30-2

Graphic Log	Location: See Exploration Plan Latitude: 35.6319° Longitude: -89.4129° Depth (Ft.) Approximate Elevation: 295 (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Strength Test				Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits	
						Test Type	Compressive Strength (psf)	Strain (%)	Confining Pressure (psi)			LL-PL-PI	Percent Fines
	POORLY GRADED SAND (SP) , fine to medium grained sand, gray, wet, medium dense (<i>continued</i>)	36.8											
	POORLY GRADED SAND WITH CLAY (SP-SC) , fine to medium grained sand, gray, wet, medium dense to very dense	258.2											
		40		X	10-17-15 N=32					19.5			6.6
		45		X	11-21-36 N=57					19.8			6.5
		50		X	5-5-5 N=10					24.5			5.9
		51.8											
	CLAYEY SAND (SC) , fine to medium grained sand, gray, wet, loose	243.2											
		55		X	4-4-5 N=9					22.2			14.3
		60		X	7-9-15 N=24					24.8			8.6
	POORLY GRADED SAND WITH CLAY (SP-SC) , fine to medium grained, gray to dark gray, wet, medium dense to dense	238.2											
		65		X	4-7-8 N=15					24.0			9.0
		70		X	12-15-20 N=35					25.0			10.4

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P Van Winkle

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06-02-2025

Boring Completed

06-02-2025

Boring Log No. B-30-2

Graphic Log	Location: See Exploration Plan Latitude: 35.6319° Longitude: -89.4129° Depth (Ft.) Approximate Elevation: 295 (Ft.)	Depth (Ft.)	Water Level Observations	Sample Type	Field Test Results	Strength Test				Water Content (%)	Dry Unit Weight (pcf)	Atterberg Limits	
						Test Type	Compressive Strength (psf)	Strain (%)	Confining Pressure (psi)			LL-PL-PI	Percent Fines
	POORLY GRADED SAND WITH CLAY (SP-SC) , fine to medium grained, gray to dark gray, wet, medium dense to dense (continued)												
	76.8 218.2	75			13-19-23 N=42					21.9			9.1
	LEAN CLAY WITH SAND (CL) , fine to medium grained, dark gray, wet, hard												
	81.8 213.2	80			13-20-14 N=34					23.2			82.2
	LEAN CLAY (CL) , trace sand, dark gray, moist, stiff												
	86.8 208.2	85			5-4-8 N=12								
	SANDY LEAN CLAY (CL) , dark gray, moist, very stiff												
	91.8 203.2	90			6-7-9 N=16					30.7		NP	67.5
	LEAN CLAY WITH SAND (CL) , dark grayish brown, very stiff												
	100.0 195	95			5-7-10 N=17								
					9-18-8 N=26								
	Boring Terminated at 100 Feet	100											

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).
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Boring Completed

06-02-2025

Summary of Laboratory Results

Boring ID	Depth (Ft.)	Liquid Limit	Plastic Limit	Plasticity Index	% Fines	Water Content (%)
B-30-1	0-3	29	22	7	98.1	
B-30-1	5-6.5	33	20	13		23.0
B-30-1	7.5-9					30.6
B-30-1	10-12	47	17	30	97.2	23.2
B-30-1	14.5-16	34	13	21		
B-30-1	17-18.5					29.0
B-30-1	19.5-21	28	20	8		26.3
B-30-1	23.5-25					23.5
B-30-1	28.5-30					19.5
B-30-1	33.5-35				59.5	
B-30-1	38.5-40	NP	NP	NP	10.9	22.7
B-30-1	43.5-45				4.9	23.1
B-30-1	48.5-50				5.8	18.0
B-30-1	53.5-55				7.7	25.6
B-30-1	58.5-60				9.7	23.8
B-30-1	63.5-65				10.2	21.8
B-30-1	68.5-70				9.4	23.0
B-30-1	73.5-75				9.9	21.0
B-30-1	78.5-80				18.5	25.5

Summary of Laboratory Results

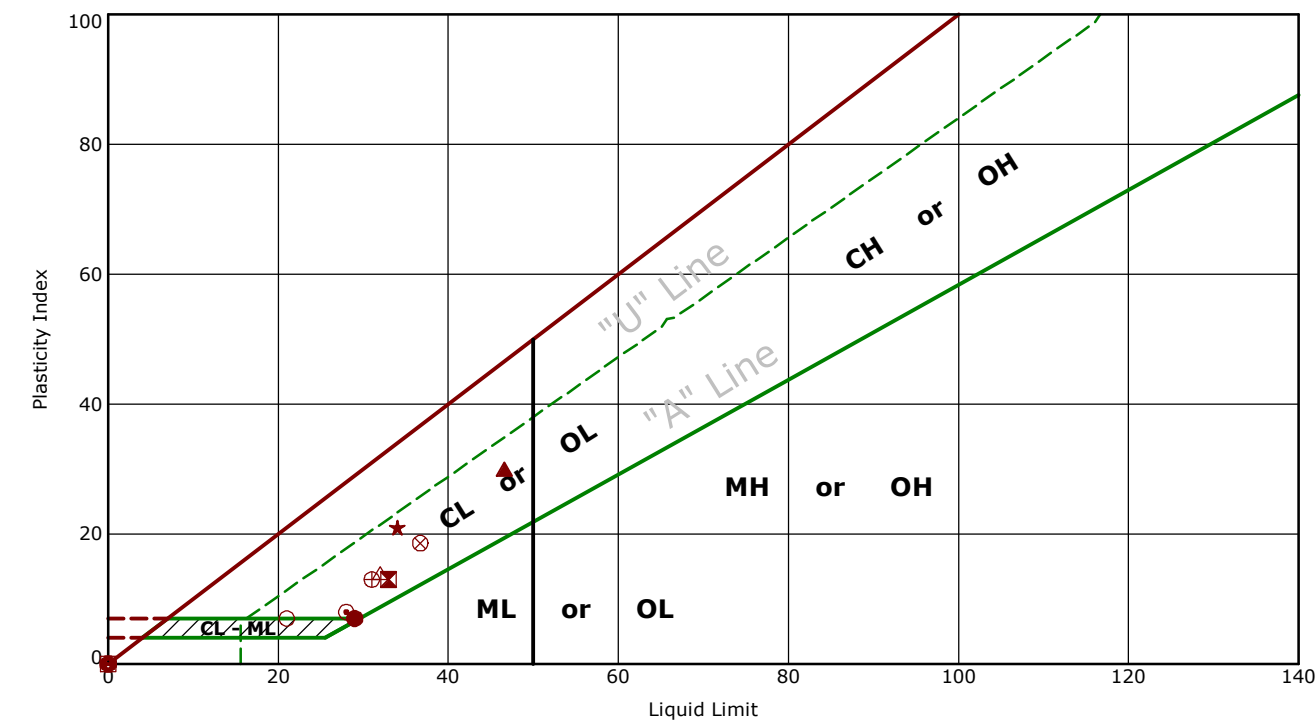
Boring ID	Depth (Ft.)	Liquid Limit	Plastic Limit	Plasticity Index	% Fines	Water Content (%)
B-30-1	83.5-85				9.6	22.9
B-30-1	88.5-90				57.9	23.8
B-30-1	98.5-100	21	14	7	67.0	27.2
B-30-2	2.5-4					27.4
B-30-2	5-6.5					26.9
B-30-2	7.5-9	32	18	14		29.2
B-30-2	12.5-14.5	37	18	19	93.3	24.7
B-30-2	14.5-16					28.3
B-30-2	17-18.5	31	18	13		26.7
B-30-2	19.5-21					25.7
B-30-2	23.5-25	NP	NP	NP		18.7
B-30-2	28.5-30				4.8	19.7
B-30-2	33.5-35				1.2	21.5
B-30-2	38.5-40				6.6	19.5
B-30-2	43.5-45				6.5	19.8
B-30-2	48.5-50				5.9	24.5
B-30-2	53.5-55				14.3	22.2
B-30-2	58.5-60				8.6	24.8
B-30-2	63.5-65				9.0	24.0

Summary of Laboratory Results

Boring ID	Depth (Ft.)	Liquid Limit	Plastic Limit	Plasticity Index	% Fines	Water Content (%)
B-30-2	68.5-70				10.4	25.0
B-30-2	73.5-75				9.1	21.9
B-30-2	78.5-80				82.2	23.2
B-30-2	88.5-90	NP	NP	NP	67.5	30.7

Atterberg Limit Results

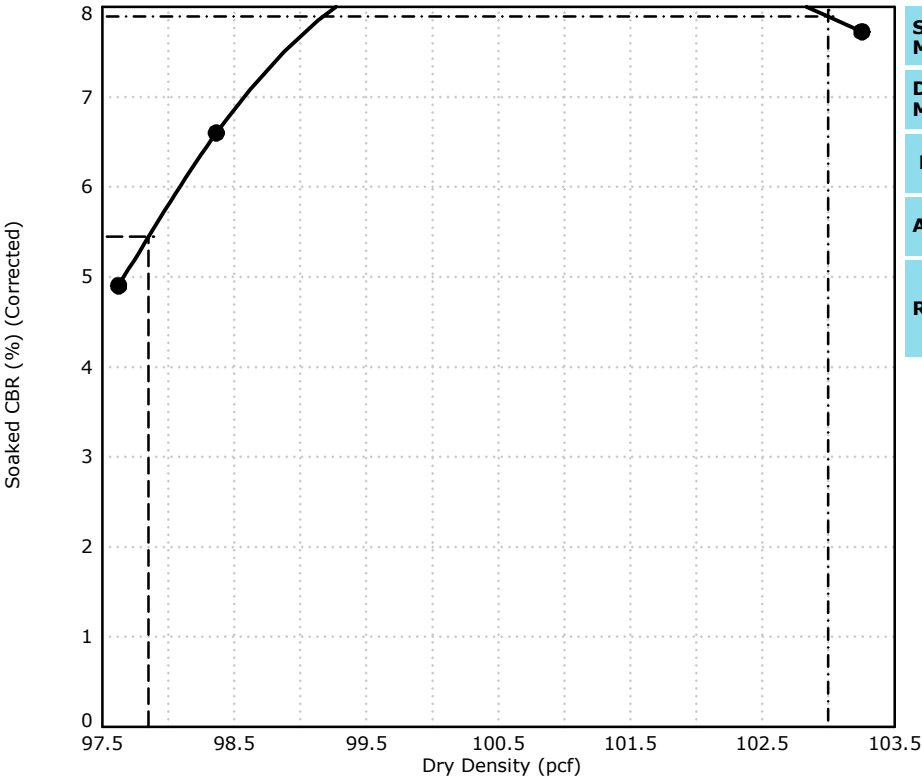
ASTM D4318



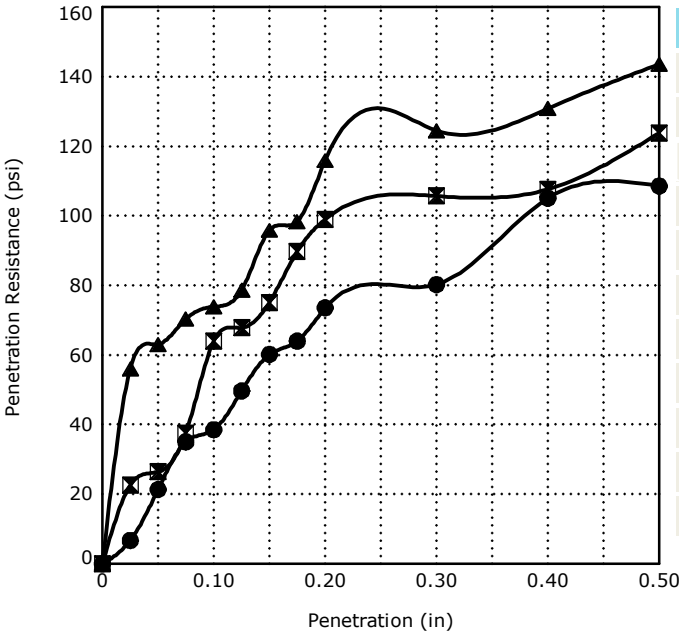
	Boring ID	Depth (Ft)	LL	PL	PI	Fines	USCS	Description
●	B-30-1	0 - 3	29	22	7	98.1	CL-ML	SILTY CLAY
⊠	B-30-1	5 - 6.5	33	20	13			
▲	B-30-1	10 - 12	47	17	30	97.2	CL	LEAN CLAY
★	B-30-1	14.5 - 16	34	13	21			
⊙	B-30-1	19.5 - 21	28	20	8			
⊕	B-30-1	38.5 - 40	NP	NP	NP	10.9		
○	B-30-1	98.5 - 100	21	14	7	67.0	CL-ML	SANDY SILTY CLAY
△	B-30-2	7.5 - 9	32	18	14			
⊗	B-30-2	12.5 - 14.5	37	18	19	93.3	CL	LEAN CLAY
⊕	B-30-2	17 - 18.5	31	18	13			
□	B-30-2	23.5 - 25	NP	NP	NP			
⊕	B-30-2	88.5 - 90	NP	NP	NP	67.5	ML	SANDY SILT

California Bearing Ratio

ASTM D1883-07²



Source of Material	B-30-1 0.0-3.0		
Description of Material	SILTY CLAY(CL-ML)		
Percent Fines	98.1		
Atterberg Limits	$\frac{LL}{29}$	$\frac{PL}{22}$	$\frac{PI}{7}$
Remarks:			



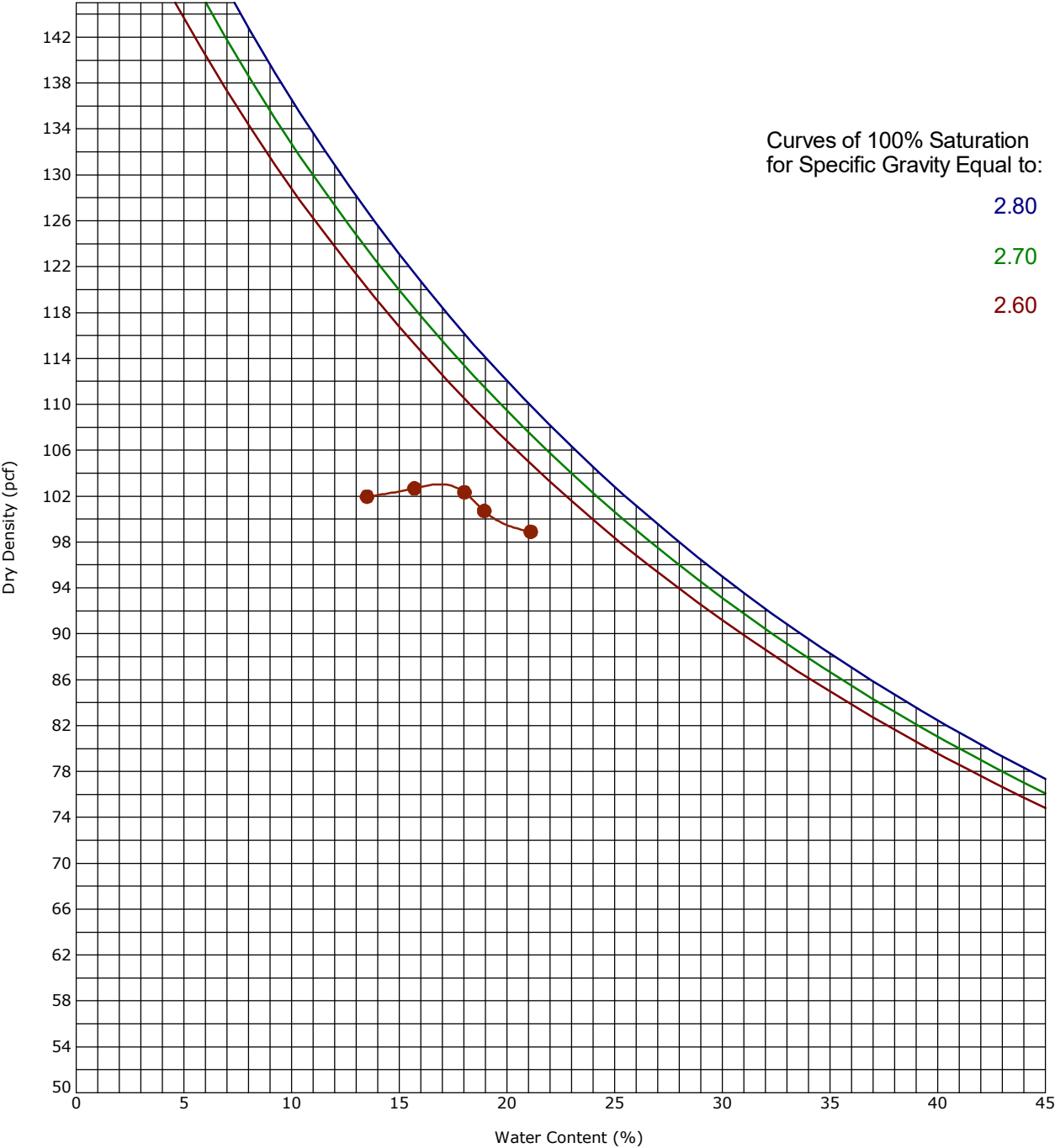
Sample No.	1	2	3
Sample Condition	Soaked		
Compaction Method	ASTM 698B		
Maximum Dry Density (pcf)	103	103	103
Optimum Moisture Content (%)	16.9	16.9	16.9
Dry Density before Soaking, (pcf)	97.62	98.36	103.25
Moisture Content, (%)			
After Compaction	16.8	16.8	16.8
Top 1" After Soaking	22.4	20.7	19.8
Surcharge, (lbs)	10.07	10.00	9.99
Swell, (%)	-0.35	0.75	0.55
Bearing Ratio, (%)	4.9	6.6	7.7

Dry Density @ 90% 92.7 pcf
Dry Density @ 95% 97.9 pcf
Dry Density @ 100% 103.0 pcf

CBR @ 90% Density _____
CBR @ 95% Density 5.4
CBR @ 100% Density 7.9

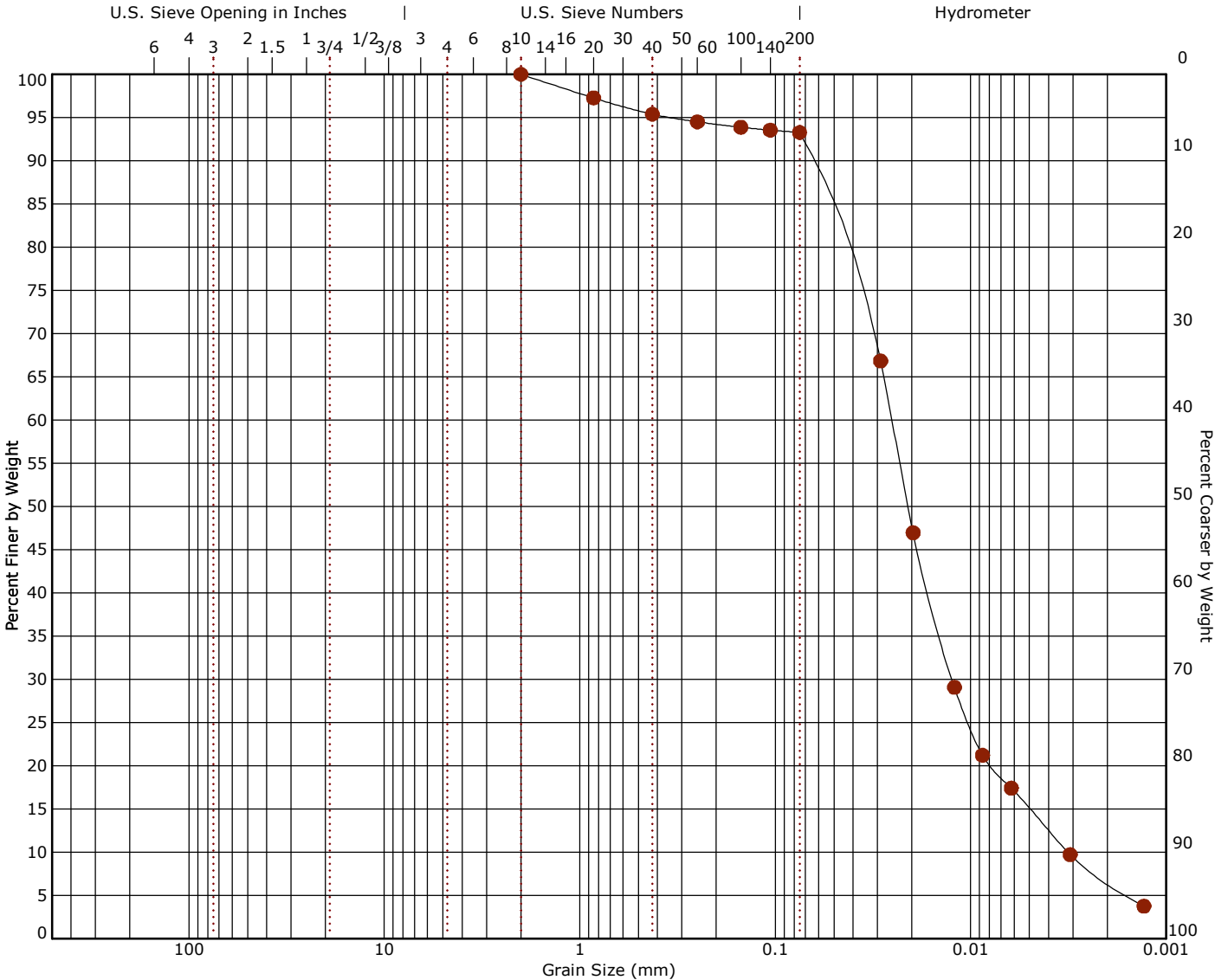
Moisture-Density Relationship

ASTM D698-Method B



Boring ID		Depth (Ft)		Description of Materials			
B-30-1		0 - 3		SILTY CLAY(CL-ML)			
Fines (%)	Fraction > mm size	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)
98	0.0	29	22	7	ASTM D698-Method B	103.0	16.9

Grain Size Distribution
ASTM D422 / ASTM C136 / AASHTO T27

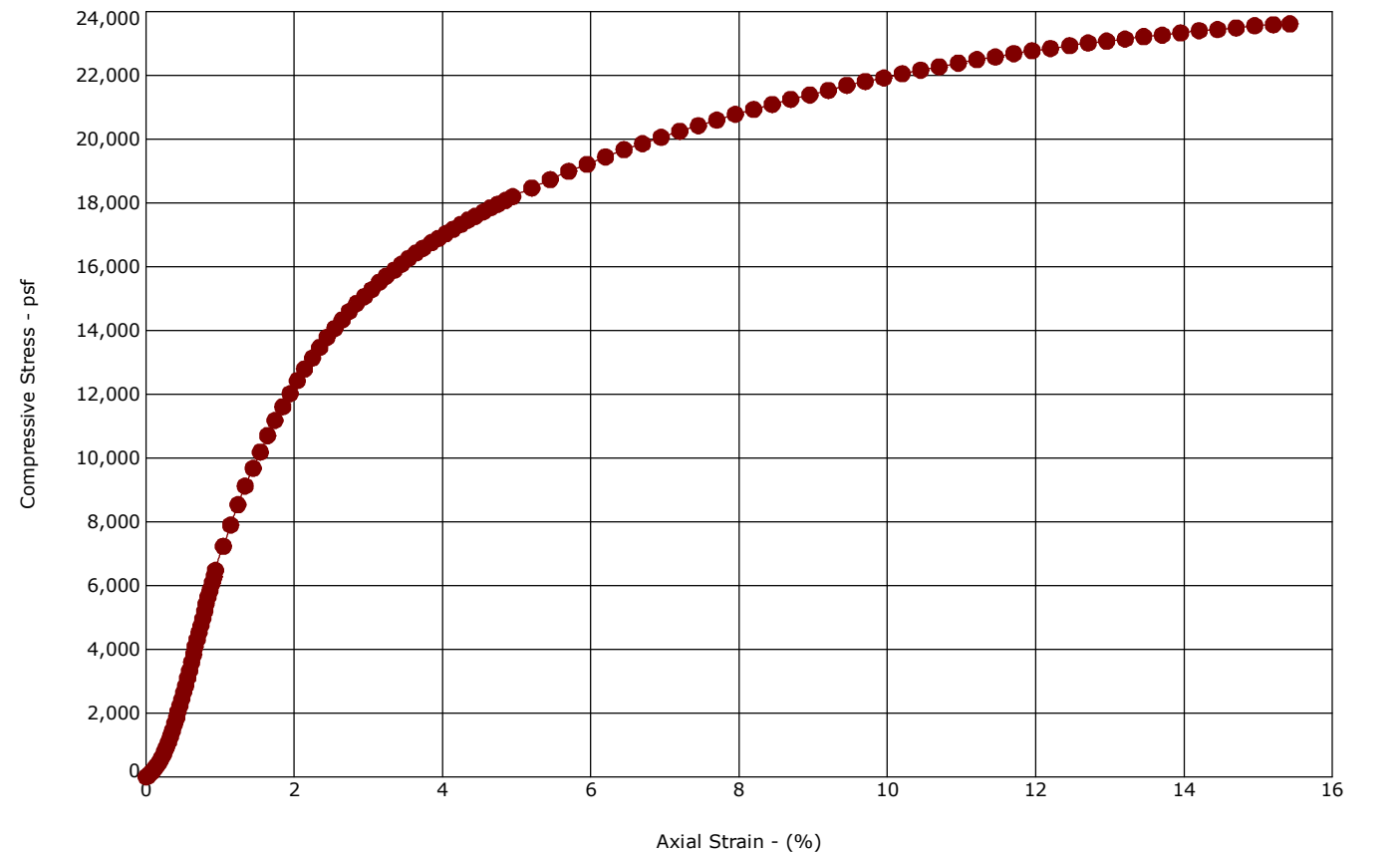


Cobbles		Gravel		Sand			Silt or Clay		
		coarse	fine	coarse	medium	fine			
Boring ID	Depth	% Cobbles	% Gravel	% Sand	% Fines	% Silt	% Clay	USCS	
● B-30-2	12.5 - 14.5	0.0	0.0	6.7		78.3	15.0	CL	

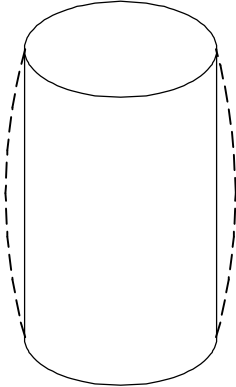
Description			●						Grain Size			
● LEAN CLAY			Sieve	% Finer	Sieve	% Finer	Sieve	% Finer		●		
			#10	100.0					D ₆₀	0.025		
			#20	97.27								
			#40	95.38								
			#60	94.5								
			#100	93.88					D ₁₀	0.003		
			#140	93.54								
			#200	93.28								
Remarks									Coefficients			
●										●		
									C _c	1.91		
									C _u	7.97		

Unconsolidated-Undrained Test

ASTM D2850



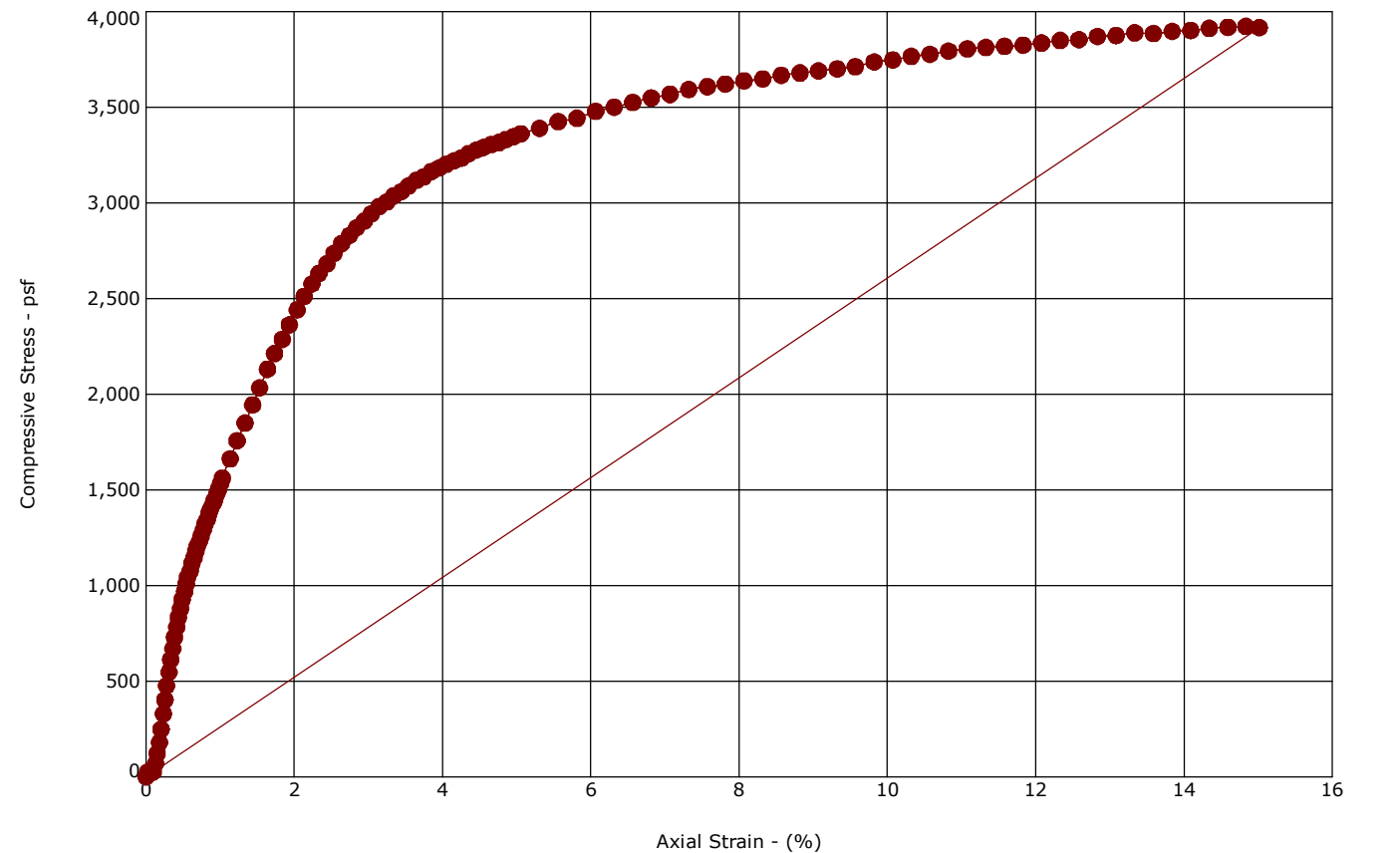
Boring ID	Depth (Ft)	Sample type	LL	PL	PI	Fines (%)	Description
B-30-1	10 - 12	Shelby Tube	47	17	30	97.2	LEAN CLAY(CL)

Specimen Failure Mode	Specimen Test Data
	Moisture Content (%): 23.2
	Dry Density (pcf) 105.1
	Diameter (in): 2.83
	Height (in): 5.66
	Height / Diameter Ratio: 2.00
	Calculated Saturation (%) 103.72
	Calculated Void Ratio: 0.60
	Assumed Specific Gravity: 2.7
	Failure Strain (%): 15.00
	Compressive Strength (psf): 23562
	Undrained Shear Strength (psf): 11781
	Strain Rate (in/min): 0.0566
	Confining Pressure (psi):
	Remarks:

Failure Mode: Bulge (dashed)

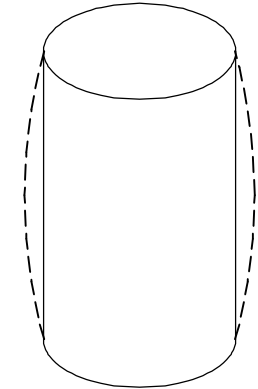
Unconsolidated-Undrained Test

ASTM D2850



Boring ID	Depth (Ft)	Sample type	LL	PL	PI	Fines (%)	Description
B-30-2	12.5 - 14.5	Shelby Tube	37	18	19	93.3	LEAN CLAY(CL)

Specimen Failure Mode	Specimen Test Data
	Moisture Content (%): 24.7
	Dry Density (pcf) 102.9
	Diameter (in): 2.82
	Height (in): 5.65
	Height / Diameter Ratio: 2.00
	Calculated Saturation (%) 104.67
	Calculated Void Ratio: 0.64
	Assumed Specific Gravity: 2.7
	Failure Strain (%): 14.84
	Compressive Strength (psf): 3923
	Undrained Shear Strength (psf): 1961
	Strain Rate (in/min): 0.0564
	Confining Pressure (psi): 10.0
	Remarks:



Failure Mode: Bulge (dashed)

Client

American Structurepoint Inc
Cleveland, OH

Project Number

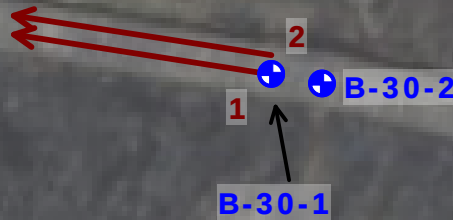
1A255072

Corrosivity Suite - Results

Sample Location		B-30-2			
Sample Depth (ft.)		10.0-11.5'			
Acidity (pH)	AASHTO T289	7.5			
Water Soluble Sulfate Ion Content (mg/Kg)	ASTM C1580	110			
Water Soluble Sulfide Content (mg/Kg)	AWWA 4500-S,D	Nil			
Water Soluble Chloride Ion Content (mg/Kg)	ASTM D512	<20			
Oxidation-Reduction Potential (RmV)	ASTM G200	88.5			
Total Dissolved Salts (mg/Kg)	AWWA 2520 B	495.5			
Electrical Resistivity ($\Omega \cdot \text{cm}$)	ASTM G57	1800			

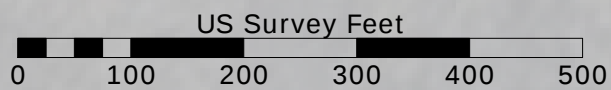
Verified By: Myles Warner
8/12/2025

These tests were performed in general accordance with the applicable AASHTO, ASTM, and AWWA test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced without the full written consent of Terracon Consultants Inc.. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar materials.



Legend

-  MASW Line Locations
-  Geotechnical Boring Locations

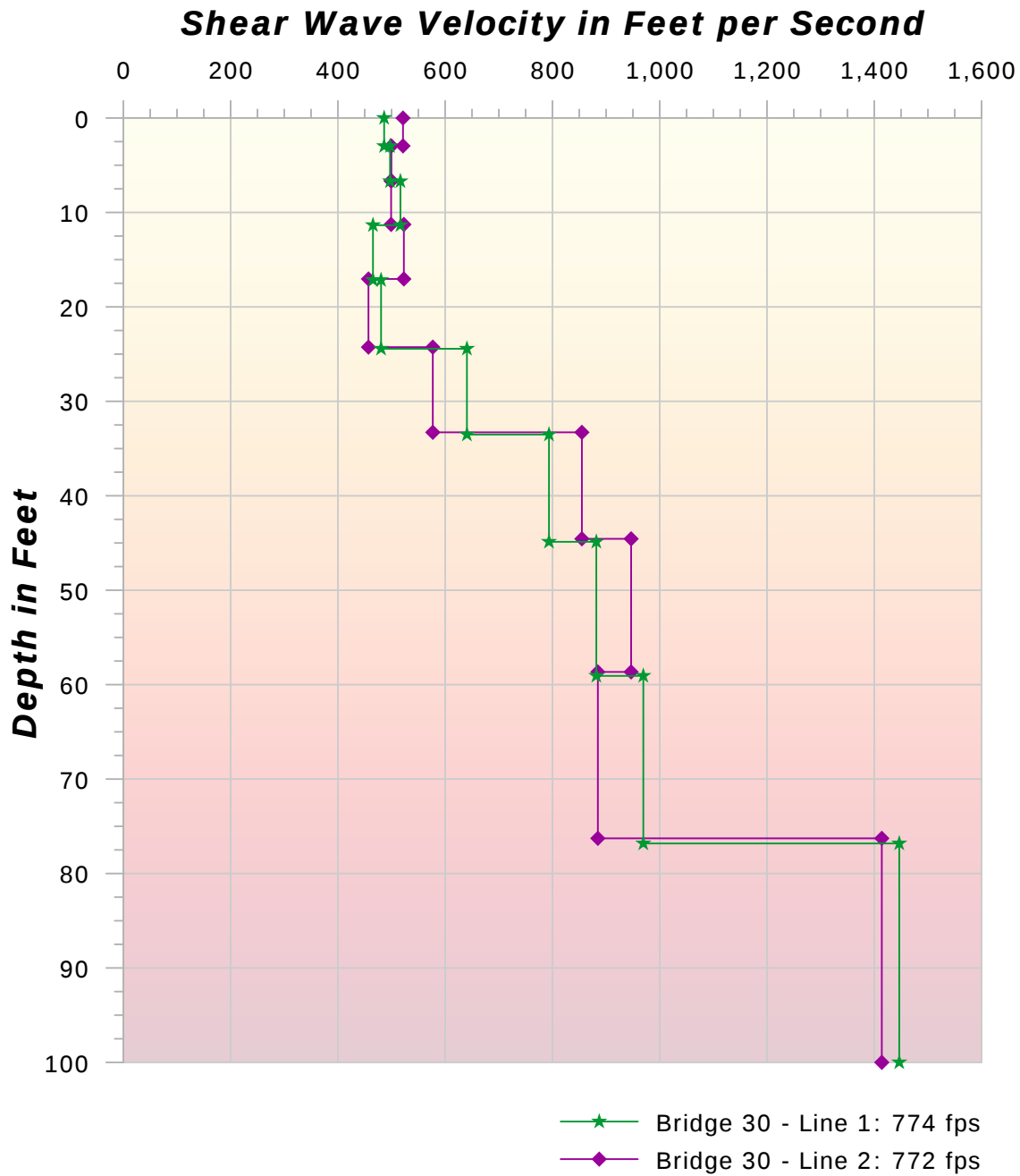


Notes

- 1) The MASW arrays performed by Terracon on May 15, 2025 are shown above in **RED**. Label locations indicate the start, or "0-foot," mark of the arrays. Several geophone locations were collected using a sub-meter accurate GPS receiver.
- 2) Geotechnical boring locations were collected using a handheld GPS and are shown above in **BLUE**.
- 3) Aerial imagery provided by Bing.

PROJECT MANAGER: ECC	PROJECT NUMBER: 1A255072	 1922 Old Murfreesboro Pike, Suite 905 Nashville, TN 37217	Geophysical Exploration Plan	EXHIBIT
DRAWN BY: AGW	DRAWING SCALE: AS SHOWN		Replacement of Bridge 30 (SR-87 Over Lagoon Creek Overflow) Haywood County, TN	1
CHECKED BY: NBR	FILE NAME: Loc-30.srf			
APPROVED BY: DAB	DATE DRAWN: 8/7/2025			

Vs100' Model TDOT Bridge 30



Notes:

- 1) Seismic testing was conducted by Terracon on May 15, 2025.
- 2) Shear wave velocity testing and calculations were conducted in general accordance with ASCE 7-16 and IBC 2018.

PROJECT MANAGER:	ECC
DRAWN BY:	AGW
CHECKED BY:	NBR
APPROVED BY:	DAB
PROJECT NUMBER:	1A255072
PROJECT TASK:	1
FILE NAME:	Vs100.gpj
DATE:	8/7/2025



Site Classification Data
Replacement of Bridge 30 (SR-87 Over Lagoon Creek Overflow) Haywood County, TN

EXHIBIT
2

Geotechnical Data Report

Replacement of Bridge 30 (SR-87 Over Lagoon Creek Overflow) | Haywood County, Tennessee
August 15, 2025 | Terracon Project No. 1A255072



Supporting Information

Contents:

General Notes

Unified Soil Classification System

General Notes

Sampling	Water Level	Field Tests
 Grab Sample  Shelby Tube  Standard Penetration Test	 Water Initially Encountered  Water Level After a Specified Period of Time  Water Level After a Specified Period of Time  Cave In Encountered Water levels indicated on the soil boring logs are the levels measured in the borehole at the times indicated. Groundwater level variations will occur over time. In low permeability soils, accurate determination of groundwater levels is not possible with short term water level observations.	N Standard Penetration Test Resistance (Blows/Ft.) (HP) Hand Penetrometer (T) Torvane (DCP) Dynamic Cone Penetrometer UC Unconfined Compressive Strength (PID) Photo-Ionization Detector (OVA) Organic Vapor Analyzer

Descriptive Soil Classification
Soil classification as noted on the soil boring logs is based Unified Soil Classification System. Where sufficient laboratory data exist to classify the soils consistent with ASTM D2487 "Classification of Soils for Engineering Purposes" this procedure is used. ASTM D2488 "Description and Identification of Soils (Visual-Manual Procedure)" is also used to classify the soils, particularly where insufficient laboratory data exist to classify the soils in accordance with ASTM D2487. In addition to USCS classification, coarse grained soils are classified on the basis of their in-place relative density, and fine-grained soils are classified on the basis of their consistency. See "Strength Terms" table below for details. The ASTM standards noted above are for reference to methodology in general. In some cases, variations to methods are applied as a result of local practice or professional judgment.

Location And Elevation Notes
Exploration point locations as shown on the Exploration Plan and as noted on the soil boring logs in the form of Latitude and Longitude are approximate. See Exploration and Testing Procedures in the report for the methods used to locate the exploration points for this project. Surface elevation data annotated with +/- indicates that no actual topographical survey was conducted to confirm the surface elevation. Instead, the surface elevation was approximately determined from topographic maps of the area.

Strength Terms				
Relative Density of Coarse-Grained Soils (More than 50% retained on No. 200 sieve.) Density determined by Standard Penetration Resistance		Consistency of Fine-Grained Soils (50% or more passing the No. 200 sieve.) Consistency determined by laboratory shear strength testing, field visual-manual procedures or standard penetration resistance		
Relative Density	Standard Penetration or N-Value (Blows/Ft.)	Consistency	Unconfined Compressive Strength Qu (psf)	Standard Penetration or N-Value (Blows/Ft.)
Very Loose	0 - 3	Very Soft	less than 500	0 - 1
Loose	4 - 9	Soft	500 to 1,000	2 - 4
Medium Dense	10 - 29	Medium Stiff	1,000 to 2,000	5 - 8
Dense	30 - 50	Stiff	2,000 to 4,000	9 - 15
Very Dense	> 50	Very Stiff	4,000 to 8,000	16 - 30
		Hard	> 8,000	> 30

Relevance of Exploration and Laboratory Test Results
Exploration/field results and/or laboratory test data contained within this document are intended for application to the project as described in this document. Use of such exploration/field results and/or laboratory test data should not be used independently of this document.

Unified Soil Classification System

Criteria for Assigning Group Symbols and Group Names Using Laboratory Tests ^A				Soil Classification	
				Group Symbol	Group Name ^B
Coarse-Grained Soils: More than 50% retained on No. 200 sieve	Gravels: More than 50% of coarse fraction retained on No. 4 sieve	Clean Gravels: Less than 5% fines ^C	Cu≥4 and 1≤Cc≤3 ^E	GW	Well-graded gravel ^F
			Cu<4 and/or [Cc<1 or Cc>3.0] ^E	GP	Poorly graded gravel ^F
		Gravels with Fines: More than 12% fines ^C	Fines classify as ML or MH	GM	Silty gravel ^{F, G, H}
			Fines classify as CL or CH	GC	Clayey gravel ^{F, G, H}
	Sands: 50% or more of coarse fraction passes No. 4 sieve	Clean Sands: Less than 5% fines ^D	Cu≥6 and 1≤Cc≤3 ^E	SW	Well-graded sand ^I
			Cu<6 and/or [Cc<1 or Cc>3.0] ^E	SP	Poorly graded sand ^I
		Sands with Fines: More than 12% fines ^D	Fines classify as ML or MH	SM	Silty sand ^{G, H, I}
			Fines classify as CL or CH	SC	Clayey sand ^{G, H, I}
Fine-Grained Soils: 50% or more passes the No. 200 sieve	Silts and Clays: Liquid limit less than 50	Inorganic:	PI > 7 and plots above “A” line ^J	CL	Lean clay ^{K, L, M}
			PI < 4 or plots below “A” line ^J	ML	Silt ^{K, L, M}
		Organic:	$\frac{LL \text{ oven dried}}{LL \text{ not dried}} < 0.75$	OL	Organic clay ^{K, L, M, N} Organic silt ^{K, L, M, O}
	Silts and Clays: Liquid limit 50 or more	Inorganic:	PI plots on or above “A” line	CH	Fat clay ^{K, L, M}
			PI plots below “A” line	MH	Elastic silt ^{K, L, M}
		Organic:	$\frac{LL \text{ oven dried}}{LL \text{ not dried}} < 0.75$	OH	Organic clay ^{K, L, M, P} Organic silt ^{K, L, M, Q}
Highly organic soils:	Primarily organic matter, dark in color, and organic odor			PT	Peat

^A Based on the material passing the 3-inch (75-mm) sieve.

^B If field sample contained cobbles or boulders, or both, add “with cobbles or boulders, or both” to group name.

^C Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with silt, GP-GC poorly graded gravel with clay.

^D Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with silt, SP-SC poorly graded sand with clay.

^E $Cu = D_{60}/D_{10}$ $Cc = \frac{(D_{30})^2}{D_{10} \times D_{60}}$

^F If soil contains ≥ 15% sand, add “with sand” to group name.

^G If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

^H If fines are organic, add “with organic fines” to group name.

^I If soil contains ≥ 15% gravel, add “with gravel” to group name.

^J If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.

^K If soil contains 15 to 29% plus No. 200, add “with sand” or “with gravel,” whichever is predominant.

^L If soil contains ≥ 30% plus No. 200 predominantly sand, add “sandy” to group name.

^M If soil contains ≥ 30% plus No. 200, predominantly gravel, add “gravelly” to group name.

^N PI ≥ 4 and plots on or above “A” line.

^O PI < 4 or plots below “A” line.

^P PI plots on or above “A” line.

^Q PI plots below “A” line.

